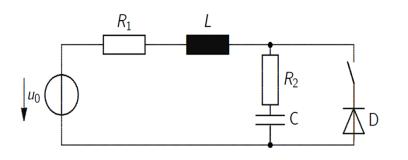


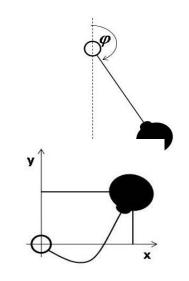
Comparison of Approaches for Modelling and Simulation of Structural-dynamic Systems – ARGESIM Benchmark C21 'State Events and Structural-

Andeas Körner, Felix Breitenecker

Mathematical Modelling and Simulation Group
Institute for Analysis and Scientific
Computing, TU Wien, Austria

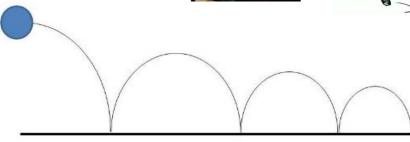
dynamic Systems'





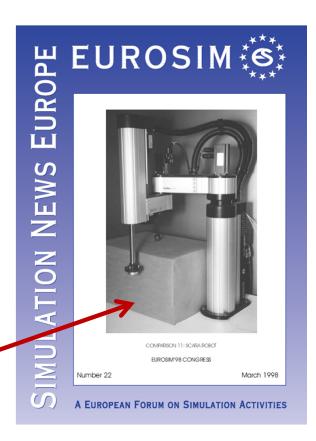








- C1 Lithium-Cluster Dynamics, SNE 0(1), 1990
- C2 Flexible Assembly System, SNE 1(1), 1991
- C3 Generalized Class-E Amplifier, SNE 1(2), 1991
- C4 Dining Philosophers I, SNE 1(3), 1991
- C5 Two State Model, SNE 2(1), 1992
- C6 Emergency Department SNE 2(3), 1992
- C7 Constrained Pendulum, SNE 3(1), 1993
- CP1 Parallel Simulation Techniques, SNE 4(1), 1994
- C8 Canal-and-Lock System, SNE 6(1), 1996
- C9 Fuzzy Control of a Two Tank System, SNE 6(2), 1996
- C10 Dining Philosophers II, SNE 6(3), 1996
- C11 SCARA Robot, SNE 8(1), 1998



Comparison of Simulation Software →



C12 Collision of Spheres, SNE 9(3), 1999

C13 Crane Crab and Embedded Control, SNE 11(1), 2001

C14 Supply Chain, SNE 11(2-3), 2001

C15 Clearance Identification, SNE 12(2-3), 2002

C16 Restaurant Business Dynamics, SNE 14(1), 2004

C17 Spatial Dynamics of SIR Epidemics, SNE 14(2-3), 2004;

C18 Neural Networks vs. Transfer Functions, SNE 15(1), 2005

C19 Pollution in Groundwater Flow, SNE 15(2-3), 2005

CP2 Parallel & Distributed Simulation, SNE 16(2), 2006





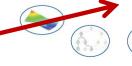






Parallel and Distributed Simulation Methods and Environments







Volume 16 Number 2

September 2006, ISSN 0929-2268



... → Benchmarks for Modelling Approaches and Simulation Implementations



C17 Spatial Dynamics of SIR Epidemics, rev. SNE 25(2), 2015

C18 Neural Networks vs. Transfer Functions, SNE 15(1), 2005

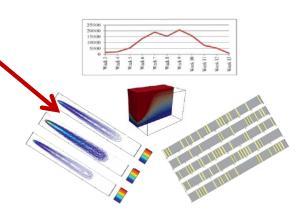
C19 Pollution in Groundwater Flow, rev. SNE 16(3-4), 2006

CP2 Parallel & Distributed Simulation, SNE 16(2), 2006

C20 Complex Assembly System, SNE 21(3-4), 2011

- SNE is publishing revised definitions
- Extended solution documentation (> 1 page)
- Extended Benchmarks: SNE introduces extended
 benchmarks, comparing modelling and simulation
 paradigms, or dealing with more complex models and experiments
- Documentation and publication in SNE of 'solutions' may take more pages – up to 10 pages SNE.





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Trends in Modelling and Simulation

Membership Journal for Simulation

Societies and Groups in FUROSIM





C17 Spatial Dynamics of SIR Epidemics, rev. SNE 25(2), 2015

C18 Neural Networks vs. Transfer Functions, SNE 15(1), 2005

C19 Pollution in Groundwater Flow, rev. SNE 16(3-4), 2006

CP2 Parallel & Distributed Simulation, SNE 16(2), 2006

C20 Complex Assembly System, SNE 21(3-4), 2011



















SNE EUROSIM Congress Issue

Volume 26 No.2 June 2016

doi: 10.11128/sne.26.2.1033



Trends in Modelling and Simulation
Membership Journal for Simulation



Print ISSN 2305-9974

C21 State Events and Structural-dynamic Systems, SNE 26(2), 2016

Benchmarks for Modelling Approaches and Simulation Implementations



DEVELOPMENT OF SYSTEM SIMULATION

$$\dot{\vec{x}}(t) = \dot{f}(t, \vec{x}(t), \vec{u}(t)),$$

$$\vec{x}(t_0) = x_0,$$





$$\dot{\vec{x}}(t) = \vec{f}(t, \vec{x}(t), \vec{z}(t), \vec{u}(t), \vec{p}), \qquad \vec{x}(t_0) = x_0$$

$$\vec{g}(\vec{x}(t), \vec{z}(t), \vec{u}(t), \vec{p}) = \vec{0}$$

DAE

$$h^{B}(\vec{x}(t), \vec{u}(t), \vec{p}) \stackrel{!}{=} \stackrel{\hat{t}^{B}}{0} \Rightarrow E^{B}(\vec{x}(\hat{t}^{B}), \vec{u}(\hat{t}^{B}), \vec{p})$$

State Events

DEVELOPMENT OF SYSTEM SIMULATION

$$\dot{\vec{x}}(t) = \vec{f}(t, \vec{x}(t), \vec{z}(t), \vec{u}(t), \vec{p}), \quad \vec{x}(t_0) = x_0$$

$$\vec{g}(\vec{x}(t), \vec{z}(t), \vec{u}(t), \vec{p}) = \vec{0}$$

$$! \pm \hat{t}^B$$

$$h^B(\vec{x}(t), \vec{u}(t), \vec{p}) = \vec{0} \Rightarrow E^B(\vec{x}(\hat{t}^B), \vec{u}(\hat{t}^B), \vec{p})$$
The property of t

- Parameter change event SE-P
- Input change event SE-I
- State change event SE-X
- Function change event SE-F
- Structure change event SE-S
- Output trace event SE-O
- Algorithm event SE-A

Event function Event action

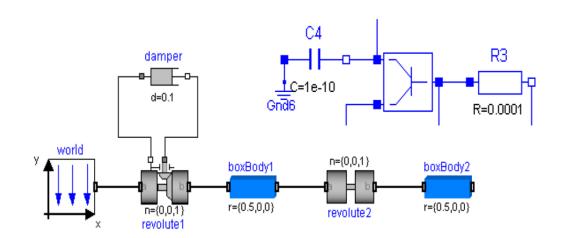


DEVELOPMENT OF SYSTEM SIMULATION

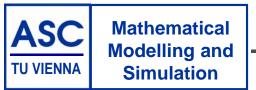
$$\dot{\vec{x}}(t) = \vec{f}(t, \vec{x}(t), \vec{z}(t), \vec{u}(t), \vec{p}), \qquad \vec{x}(t_0) = x_0$$

$$\vec{g}(\vec{x}(t), \vec{z}(t), \vec{u}(t), \vec{p}) = \vec{0}$$
State Events
$$! \pm \hat{t}^B \qquad \text{Event function}$$

$$h^B(\vec{x}(t), \vec{u}(t), \vec{p}) = \vec{0} \Rightarrow E^B(\vec{x}(\hat{t}^B), \vec{u}(\hat{t}^B), \vec{p}) \qquad \text{Event action}$$



Physical Modelling – State Space ,unknown'



STATE EVENT HANDLING

$$\dot{\vec{x}}(t) = \vec{f}(t, \vec{x}(t), \vec{z}(t), \vec{u}(t), \vec{p}), \quad \vec{x}(t_0) = x_0
\vec{g}(\vec{x}(t), \vec{z}(t), \vec{u}(t), \vec{p}) = \vec{0} \quad \text{DAE}
\underbrace{! \pm_{\hat{t}^B}}_{h^B(\vec{x}(t), \vec{u}(t), \vec{p})} = \overset{! \pm_{\hat{t}^B}}{0 \Rightarrow E^B(\vec{x}(\hat{t}^B), \vec{u}(\hat{t}^B), \vec{p})} \quad \text{State Events}$$

- Parameter change event SE-P
- Input change event SE-I
- State change event SE-X
- Function change event SE-F
- Structure change event SE-S
- Output trace event SE-O
- Algorithm event SE-A

Structural-dynamic Systems

STATE EVENT HANDLING

$$h^{B}(\vec{x}(t), \vec{u}(t), \vec{p}) = \vec{0} \Rightarrow E^{B}(\vec{x}(\hat{t}^{B}), \vec{u}(\hat{t}^{B}), \vec{p})$$

State Events

- Parameter change event SE-P
- Input change event SE-I
- State change event SE-X
- Function change event SE-F
- Structure change event SE-S
- Output trace event SE-O
- Algorithm event SE-A

Structural-dynamic Systems

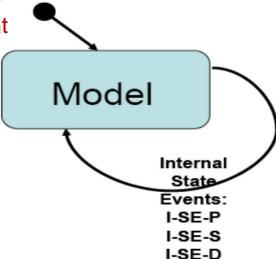
- 1. Detection of the event
- 2. Localisation of event
- 3. Event Action
- 4. Restart of solver



Structural-dynamic Systems

$$h^{B}(\vec{x}(t), \vec{u}(t), \vec{p}) \stackrel{! \pm}{=} \vec{0} \stackrel{\hat{t}^{B}}{\Rightarrow} E^{B}(\vec{x}(\hat{t}^{B}), \vec{u}(\hat{t}^{B}), \vec{p})$$
...

- Parameter change event –
- Input change event
- State change event
- Function change event
- Structure change event
- Output trace event
- Algorithm event



- 1. Detection of the event
- 2. Localisation of event
- 3. Event Action
- 4. Restart of solver

A. Körner, F. Breitenecker

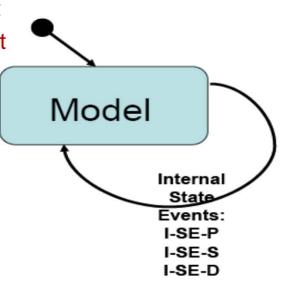
ASIM GMMS/STS Ulm March 2017



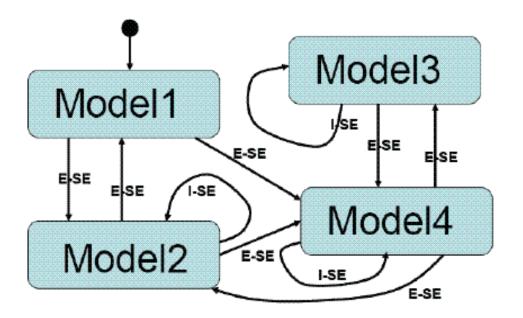
Structural-dynamic Systems

$$h^{B}(\vec{x}(t), \vec{u}(t), \vec{p}) \stackrel{! \pm}{=} \vec{0} \stackrel{\hat{\tau}^{B}}{\Rightarrow} E^{B}(\vec{x}(\hat{t}^{B}), \vec{u}(\hat{t}^{B}), \vec{p})$$
...

- Parameter change event –
- Input change event
- State change event
- Function change event
- Structure change event
- Output trace event
- Algorithm event

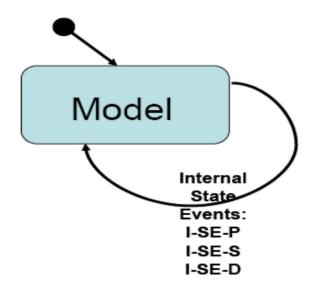


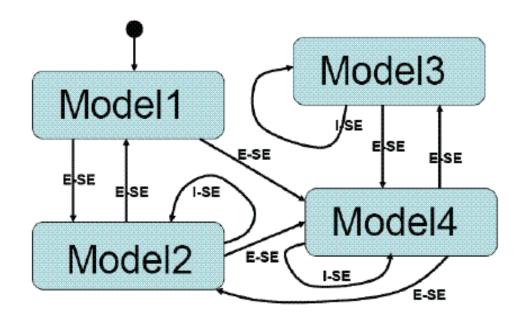
- 1. Detection of the event
- 2. Localisation of event
- 3. Event Action
- 4. Restart of solver

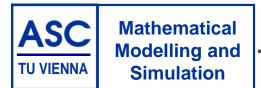




3 Case Studies

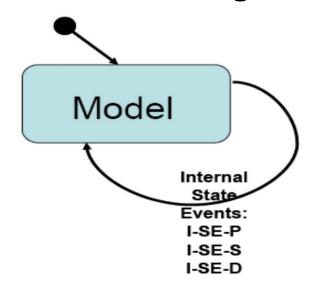


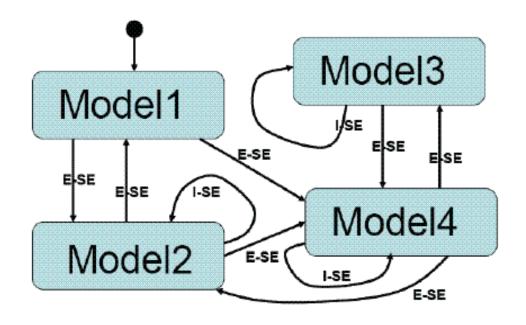




3 Case Studies

Bouncing Ball

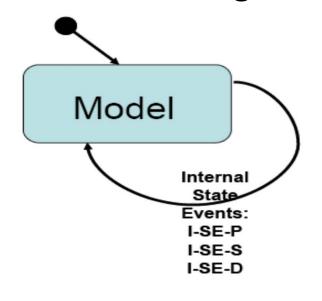




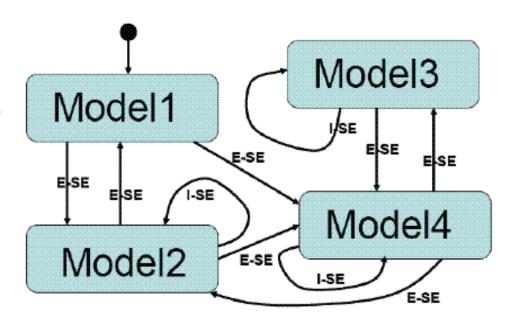


3 Case Studies

Bouncing Ball



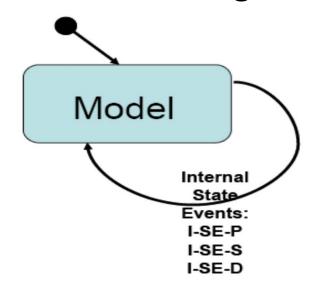
RLC Circuit with Diode



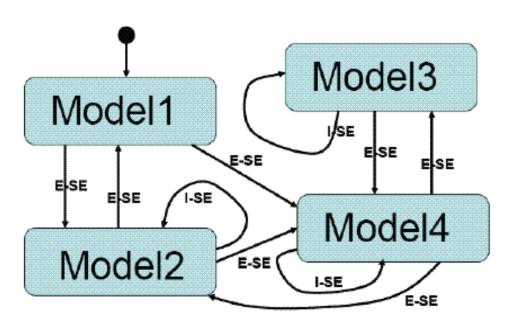


3 Case Studies

Bouncing Ball



RLC Circuit with Diode



Rotating Pendulum with Free Flight Phase



Bouncing Ball







A. Körner, F. Breitenecker

ASIM GMMS/STS Ulm March 2017



Bouncing Ball

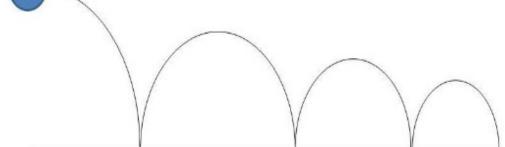






Bouncing Ball Model- Event Contact

$$\dot{x} = v, \dot{v} = -g - \beta v^2 \operatorname{sign}(v)$$





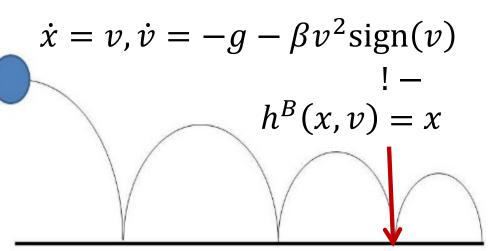
Bouncing Ball







Bouncing Ball Model- Event Contact



$$v_{new}(\hat{t}) \stackrel{\hat{t}}{\rightarrow} -\mu \cdot v_{prev}(\hat{t}).$$



Bouncing Ball

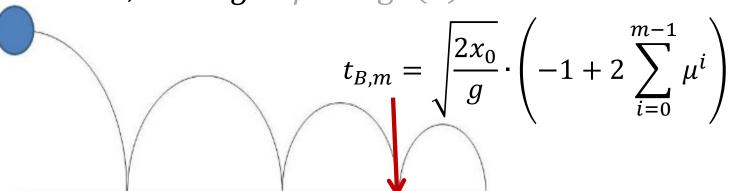






Bouncing Ball Model- Event Contact

$$\dot{x} = v, \dot{v} = -g - \beta v^2 \text{sign}(v)$$



Bouncing Ball

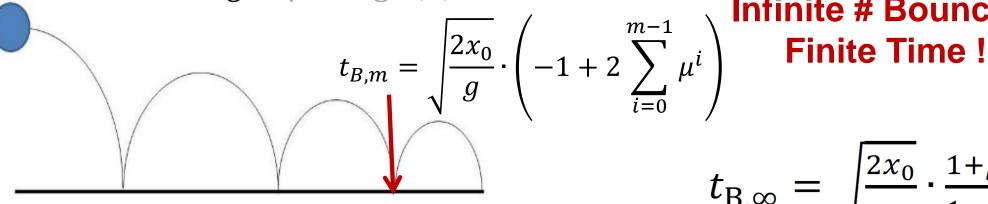






Bouncing Ball Model - Event Contact

$$\dot{x} = v, \dot{v} = -g - \beta v^2 \text{sign}(v)$$



Infinite # Bounces-

$$t_{\rm B,\infty} = \sqrt{\frac{2x_0}{g}} \cdot \frac{1+\mu}{1-\mu}$$



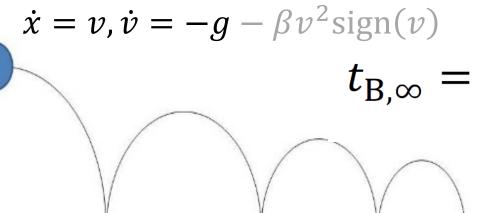
Bouncing Ball





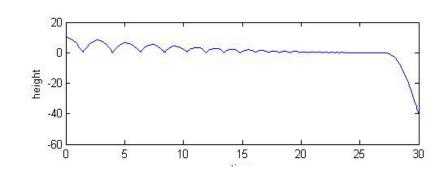


Bouncing Ball Model- Event Contact



$\sqrt{\frac{2x_0}{g} \cdot \frac{1+\mu}{1-\mu}}$

Infinite # Bounces-Finite Time





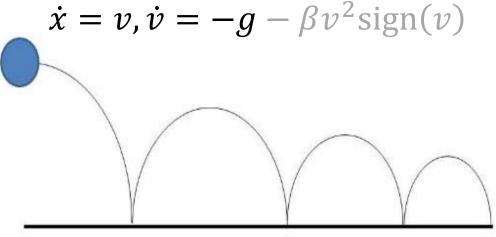
Bouncing Ball



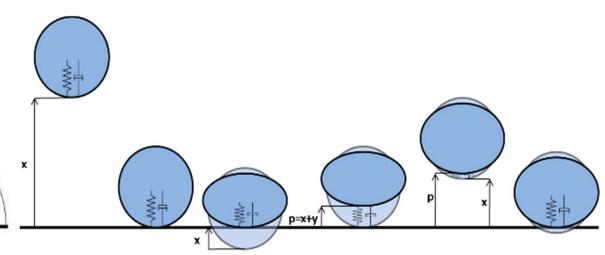




Bouncing Ball Model - Event Contact



Bouncing Ball Model -Dynamic Contact



Bouncing Ball







Flying Phase

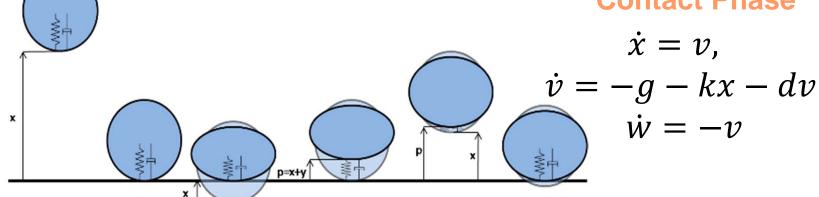
$$\dot{x} = v$$

$$\dot{v} = -g - \beta v^2 \text{sign}(v)$$

$$\dot{w} = -\frac{k}{d} \cdot w$$

Bouncing Ball Model -Dynamic Contact

Contact Phase





Bouncing Ball







Flying Phase

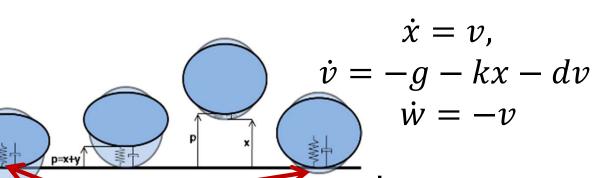
$$\dot{x} = v$$

$$\dot{v} = -g - \beta v^2 \text{sign}(v)$$

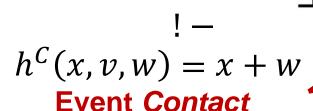
$$\dot{w} = -\frac{k}{d} \cdot w$$



Contact Phase

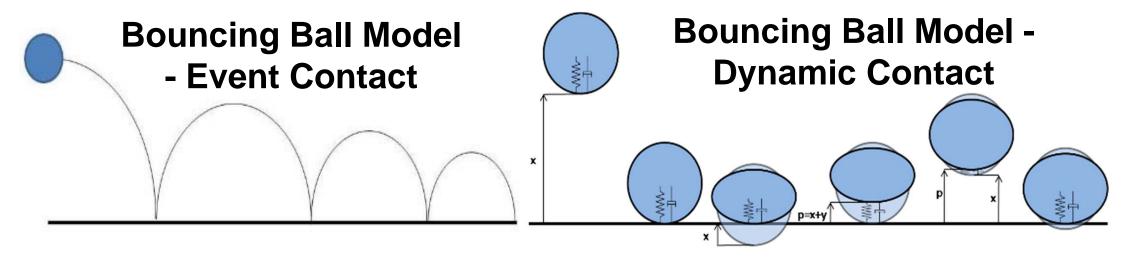


 $h^{F}(x, v, w) = -kx - dv$ Event Fly Restart





Bouncing Ball - Tasks

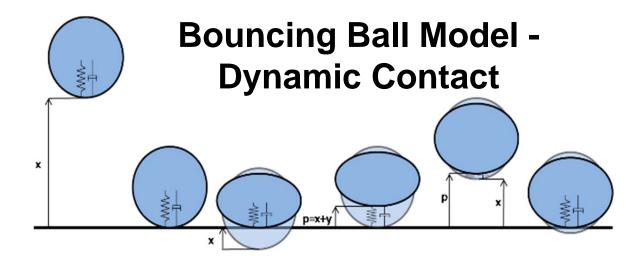


- Description of model implementation
- Simulation until last bounce scattering prevention
- Testing accuracy of event handling
- Compensation of linear model deviation.

- Description of model implementation
- Dependency of results from algorithms.
- Investigation of contact phase
- Parameter studies.



Bouncing Ball - Tasks



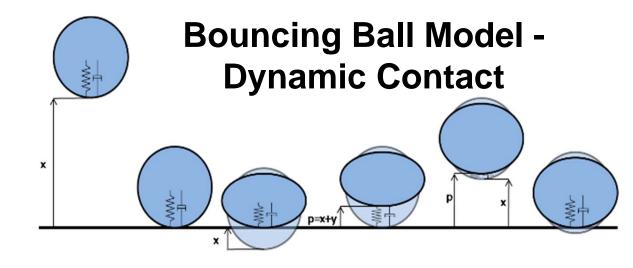
- Description of model implementation
- Dependency of results from algorithms.
- Investigation of contact phase
- Parameter studies.
- Bouncing ball on Mars.



Bouncing Ball - Tasks



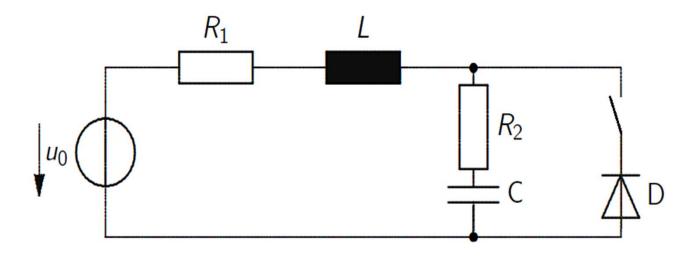
- In a publication of NASA, there was a speculation of a big inflatable ball, which can be used to damp down the impact of a lander at atmospheric entry.
- http://saturn.astrobio.net/pressrelease/63/



- Description of model implementation
- Dependency of results from algorithms.
- Investigation of contact phase
- Parameter studies.
- Bouncing ball on Mars.



RLC Circuit with Diode

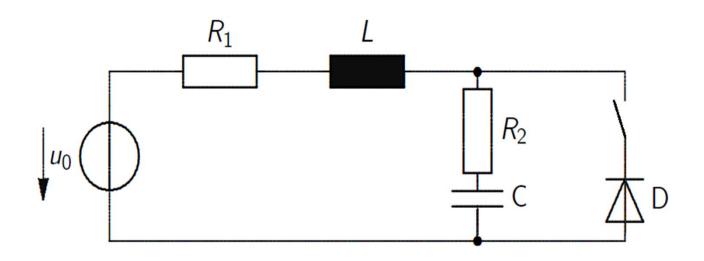


$$u_{C} + u_{R_{1}} + u_{L} + u_{R_{2}} + u_{C} = u_{0}$$

$$u_{R_{2}} + u_{C} = u_{D}$$

$$\frac{di}{dt} = \frac{1}{L}u_{L}, \qquad \frac{du_{C}}{dt} = \frac{1}{C}(i + i_{D})$$

RLC Circuit with Diode



Diode Model

$$u_D = \widehat{F}(i_D)$$

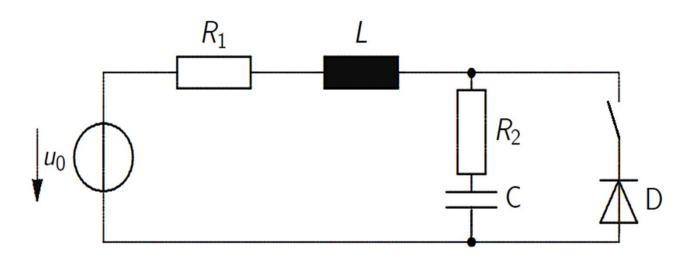
$$u_{C} + u_{R_{1}} + u_{L} + u_{R_{2}} + u_{C} = u_{0}$$

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RLC Circuit with Diode



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$$u_{R_{2}} + u_{C} = u_{D}$$

$$\frac{di}{dt} = \frac{1}{L}u_{L}, \qquad \frac{du_{C}}{dt} = \frac{1}{C}(i + i_{D})$$

Diode Model

$$u_D = \widehat{F}(i_D)$$

Locking Phase

$$i_D = 0$$
 if $u_D < 0$

Conducting Phase

$$u_D > 0$$

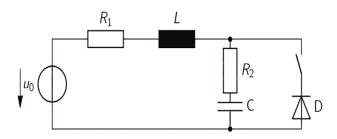
$$0 = R_2(i + i_D) + u_C - F(i_D)$$



RLC Circuit with Diode

Diode Model

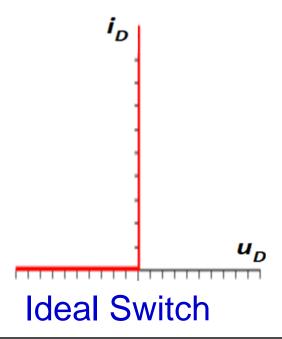
$$u_D = \widehat{F}(i_D)$$



Locking Phase

$$i_D = 0 \ if \ u_D < 0$$

$$u_D > 0$$
 $0 = R_2(i + i_D) + u_C - F(i_D)$

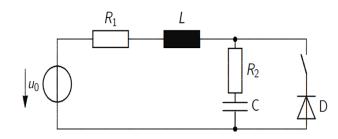




RLC Circuit with Diode

Diode Model

$$u_D = \widehat{F}(i_D)$$

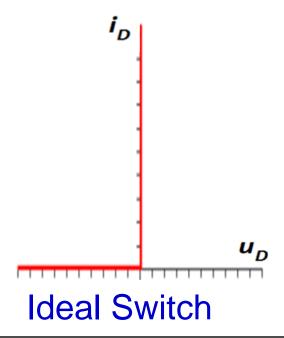


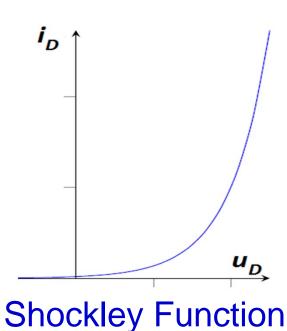
Locking Phase

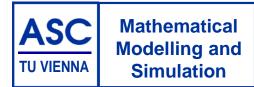
$$i_D = 0$$
 if $u_D < 0$

Conducting Phase

$$u_D > 0$$
 $0 = R_2(i + i_D) + u_C - F(i_D)$



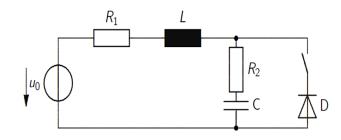




RLC Circuit with Diode

Diode Model

$$u_D = \widehat{F}(i_D)$$

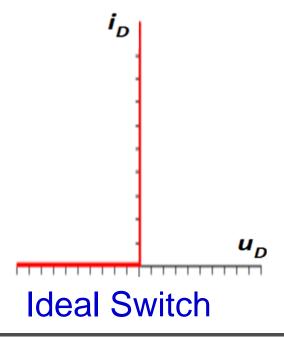


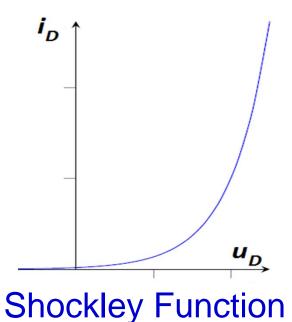
Locking Phase

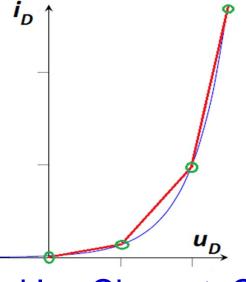
$$i_D = 0$$
 if $u_D < 0$

Conducting Phase

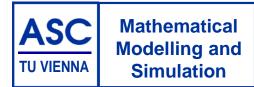
$$u_D > 0$$
 $0 = R_2(i + i_D) + u_C - F(i_D)$







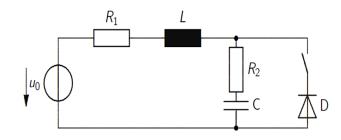
Shockley Charact. Curve



RLC Circuit with Diode

Diode Model

$$u_D = \widehat{F}(i_D)$$

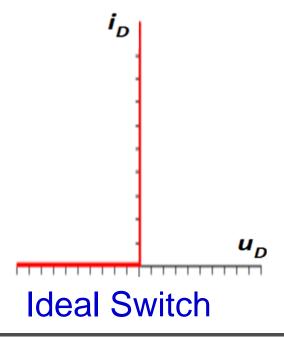


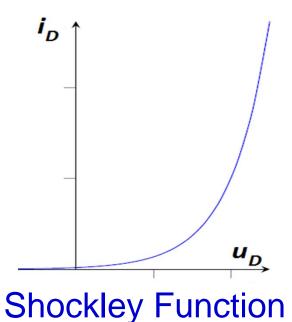
Locking Phase

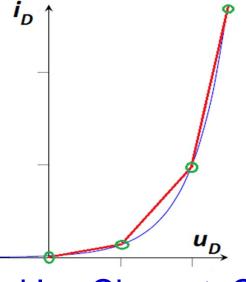
$$i_D = 0$$
 if $u_D < 0$

Conducting Phase

$$u_D > 0$$
 $0 = R_2(i + i_D) + u_C - F(i_D)$







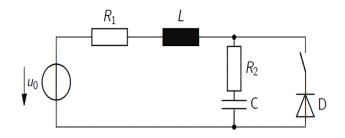
Shockley Charact. Curve



RLC Circuit with Diode

Diode Model

$$u_D = \widehat{F}(i_D)$$



Conducting Phase $u_D > 0$

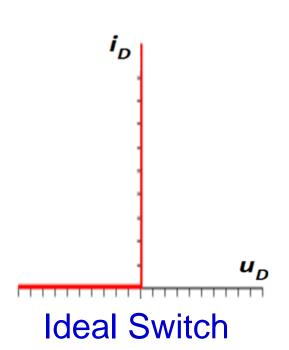
$$\frac{du_{C}}{dt} = \frac{1}{R_{2}}u_{C}, \frac{di}{dt} = -\frac{R_{1}}{L}i + \frac{1}{L}u_{0}$$

$$u_{D} = R_{2}i + u_{C}$$

Locking Phase $u_D < 0$

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$$

$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$





Mathematical Modelling and Simulation

Benchmark Structural-dynamic Systems

RLC Circuit with Diode

Diode Model

$$u_D = \widehat{F}(i_D)$$

Conducting Phase Start

$$! + h^{\mathcal{C}}(i, u_{\mathcal{C}}) = u_{\mathcal{D}} = R_2 i + u_{\mathcal{C}}$$

Locking Phase Start

$$! - h^{L}(i, u_{c}, i_{D}) = u_{D} = R_{2}(i + i_{D}) + u_{C}$$

R_1 R_2 R_2 R_2 R_2 R_3 R_4 R_5 R_5

Conducting Phase $u_D > 0$

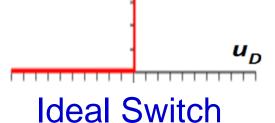
$$\frac{du_{C}}{dt} = \frac{1}{R_{2}}u_{C}, \frac{di}{dt} = -\frac{R_{1}}{L}i + \frac{1}{L}u_{0}$$

$$u_{D} = R_{2}i + u_{C}$$

Locking Phase $u_D < 0$

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$$

$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$





RLC Circuit with Diode

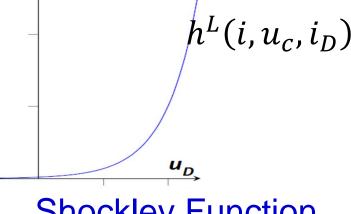
Diode Model

$$u_D = \widehat{F}(i_D)$$

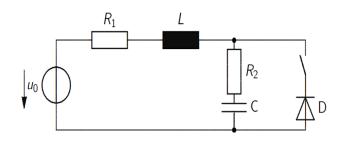
Conducting Phase Start

! +
$$h^{C}(i, u_{c}) = u_{D} = R_{2}i + u_{C}$$

Locking Phase Start



Shockley Function



Conducting Phase $u_D > 0$

 $h^L(i, u_C, i_D) = u_D = R_2(i + i_D) + u_C$ Locking Phase $u_D < 0$

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$$

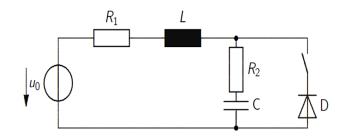
$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$



RLC Circuit with Diode

Diode Model

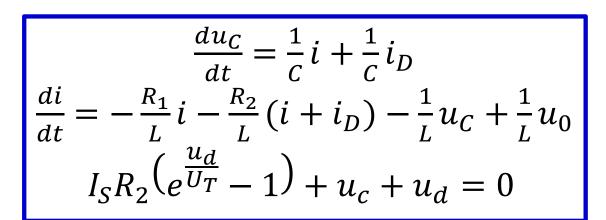
$$u_D = \widehat{F}(i_D)$$



Conducting

Phase

$$u_D > 0$$



Shockley Function

Locking Phase

$$u_D < 0$$

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$$

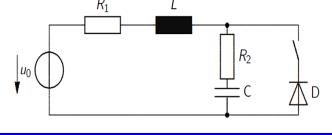
$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$



RLC Circuit with Diode

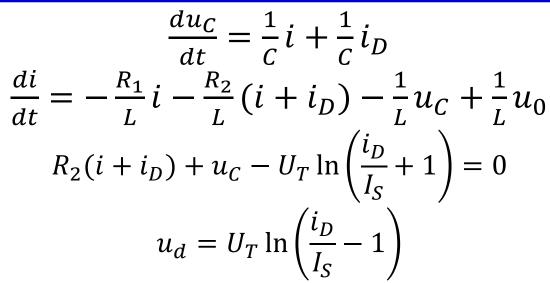
Diode Model

$$u_D = \widehat{F}(i_D)$$



Conducting Phase

$$u_D > 0$$



 u_D

Shockley Function

Locking Phase

$$u_D < 0$$

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$$

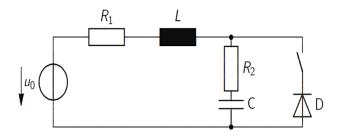
$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$



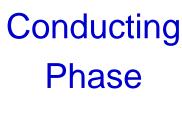
RLC Circuit with Diode

Diode Model

$$u_D = \widehat{F}(i_D)$$



$$u_D > 0$$



Locking Phase

$$u_D < 0$$

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D$$

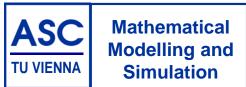
$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$

$$\dot{u}_D = -\dot{u}_C \left(I_S R_2 \left(e^{\frac{U_D}{U_T}}\right) \frac{1}{U_T} + 1\right)$$

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$$

$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$

 \boldsymbol{u}_{D}



RLC Circuit with Diode

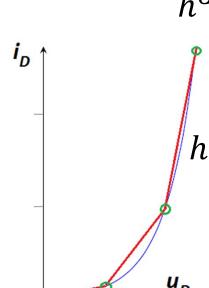
Diode Model

$$u_D = \widehat{F}(i_D)$$

Conducting Phase $u_D > 0$

Conducting Phase Start

$$! + h^{\mathcal{C}}(i, u_{\mathcal{C}}) = u_{\mathcal{D}} = R_2 i + u_{\mathcal{C}}$$



Locking Phase Start

$$h^L(i, u_C, i_D) = u_D = R_2(i + i_D) + u_C$$
 Locking Phase $u_D < 0$

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$$

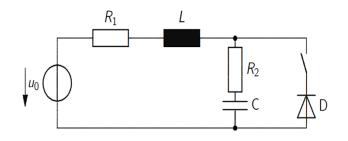
$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$



RLC Circuit with Diode

Diode Model

$$u_D = \widehat{F}(i_D)$$



Conducting

Phase

$$u_D > 0$$

 $\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D$ $\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$ $I_S R_2 \left(e^{\frac{u_d}{U_T}} - 1\right) + u_C + u_d = 0$

Locking

Phase $u_D < 0$

Shockley Charact. Curve

$$\frac{du_C}{dt} = \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$$

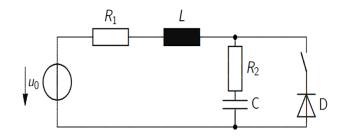
$$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$$



RLC Circuit with Diode

Diode Model

$$u_D = \widehat{F}(i_D)$$



Conducting

Phase

$$u_D > 0$$

$\frac{di}{dt} = -\frac{R_1}{L}i - \frac{R_2}{L}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$ $F_{LIN,j}(u_C(t); (u_{D,j}, i_{D,j}) + u_C + u_d = 0$

Locking Phase

 $u_D < 0$

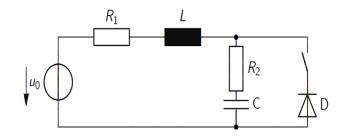
 $du_{\mathcal{C}}$ $= \frac{1}{C}i + \frac{1}{C}i_D, u_D = R_2(i + i_D) + u_C$ $= -\frac{R_1}{I}i - \frac{R_2}{I}(i + i_D) - \frac{1}{L}u_C + \frac{1}{L}u_0$

Shockley Charact. Curve

ASC TU VIENNA Mathematical Modelling and Simulation

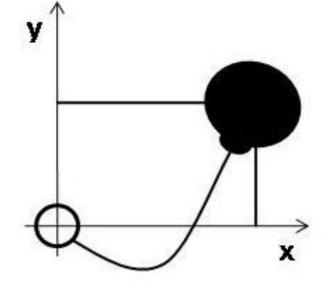
Benchmark Structural-dynamic Systems

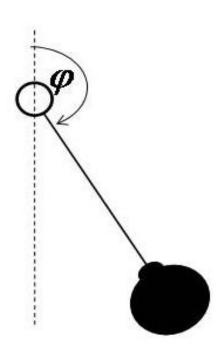
RLC Circuit with Diode - Tasks

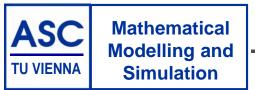


- Description of model implementations.
- Dependency of results from algorithms. (Shortcut vs Shockley)
- Comparison of Shortcut and Shockley diode model.
- Approximation of Shockley diode model (Shockley vs. Char. Curve)
- Relevance of choice of algebraic state (i_d vs u_d)
- Investigation for real-time simulation index reduction).



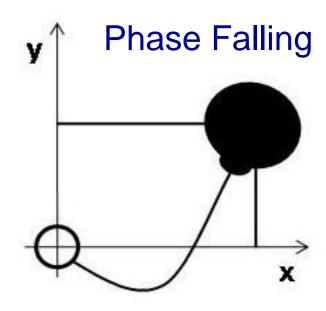


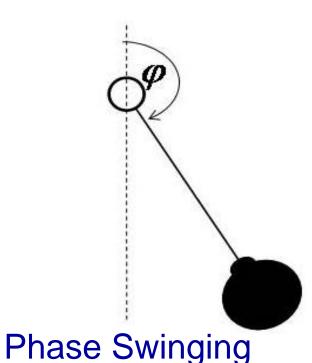




$$m\ddot{x} = -k\dot{x},$$

$$m\ddot{y} = -mg - k\dot{y}$$





$$\ddot{\varphi} + \frac{k}{m}\dot{\varphi} - \frac{g}{l}\sin(\varphi) = 0$$

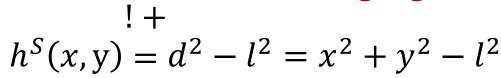


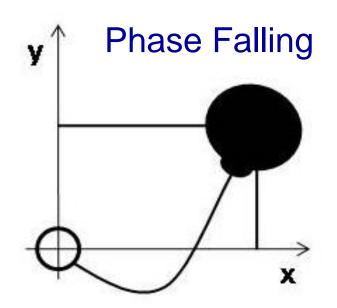
Rotating Pendulum with Free Flight Phase

$$m\ddot{x} = -k\dot{x},$$

$$m\ddot{y} = -mg - k\dot{y}$$

Event Start Swinging





$$\ddot{\varphi} + \frac{k}{m}\dot{\varphi} - \frac{g}{l}\sin(\varphi) = 0$$



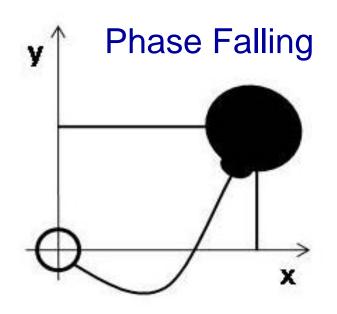
Rotating Pendulum with Free Flight Phase

$$m\ddot{x} = -k\dot{x},$$

$$m\ddot{y} = -mg - k\dot{y}$$



$$l + hS(x,y) = d2 - l2 = x2 + y2 - l2$$

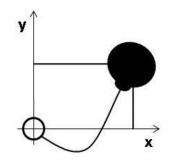


Event Start Falling $h^{F}(\varphi,\dot{\varphi}) = F = -gm\cos(\varphi) + ml\dot{\varphi}^{2}$

$$\ddot{\varphi} + \frac{k}{m}\dot{\varphi} - \frac{g}{l}\sin(\varphi) = 0$$



Rotating Pendulum with Free Flight Phase



 $\boldsymbol{\varphi}, \dot{\boldsymbol{\varphi}}, F$

circular movement

(rope tight)

$$\ddot{\boldsymbol{\varphi}} = \frac{g}{l}\sin(\boldsymbol{\varphi}) - \frac{k}{m}\dot{\boldsymbol{\varphi}}$$

$$F = -mg\cos(\boldsymbol{\varphi}) + ml\dot{\boldsymbol{\varphi}}^2$$

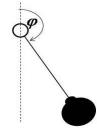


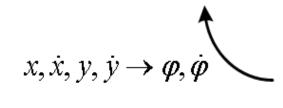
 $\varphi, \dot{\varphi} \rightarrow x, \dot{x}, y, \dot{y}$

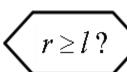
$$m\ddot{x} = -k\dot{x}$$

$$m\ddot{y} = -mg - k\dot{y}$$

$$r^2 = x^2 + y^2$$







F < 0?

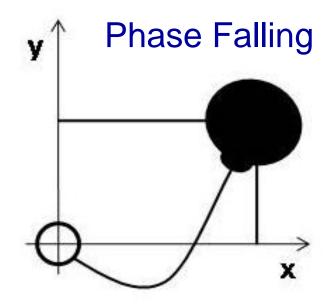
 $x, \dot{x}, y, \dot{y}, r$

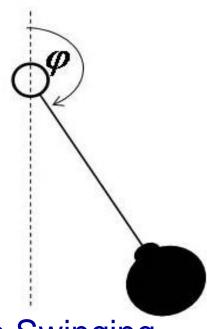


Rotating Pendulum with Free Flight Phase

$$m\ddot{x} = -k\dot{x},$$

$$m\ddot{y} = -mg - k\dot{y}$$



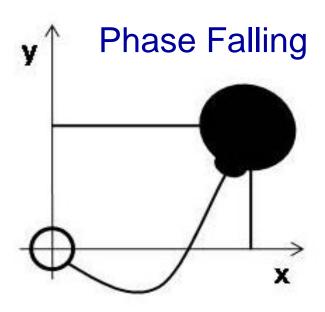


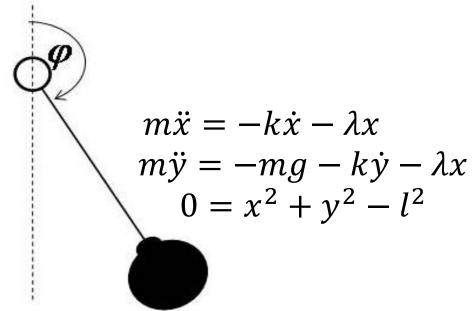


Rotating Pendulum with Free Flight Phase

$$m\ddot{x} = -k\dot{x},$$

$$m\ddot{y} = -mg - k\dot{y}$$





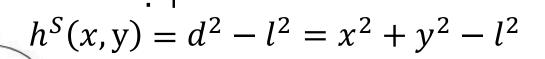


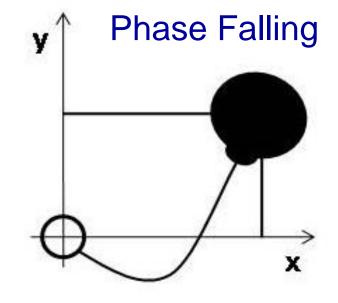
Rotating Pendulum with Free Flight

Phase

$m\ddot{x} = -k\dot{x}$ $m\ddot{y} = -mg - k\dot{y}$

Event Start Swinging





Event Start Falling

$$m\ddot{x} = -k\dot{x} - \lambda x$$

$$m\ddot{y} = -mg - k\dot{y} - \lambda x$$

$$0 = x^2 + y^2 - l^2$$

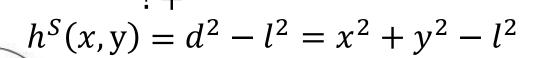
$$h^{F}(x,\dot{x},y,\dot{y}) = F = -gm \frac{y}{l} + ml \cdot f(x,\dot{x},y,\dot{y})$$

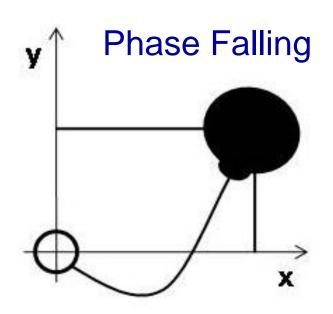


Rotating Pendulum with Free Flight Phase

ase $m\ddot{x}=-k\dot{x},$ of Start Swinging $m\ddot{y}=-mg-k\dot{y}$

Event Start Swinging





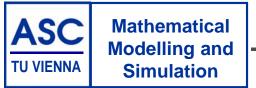
Event Start Falling

$$m\ddot{x} = -k\dot{x} - \lambda x \quad \text{DAE index 3}$$

$$m\ddot{y} = -mg - k\dot{y} - \lambda x$$

$$0 = x^2 + y^2 - l^2$$

$$h^{F}(x,\dot{x},y,\dot{y}) = F = -gm \frac{y}{l} + ml \cdot f(x,\dot{x},y,\dot{y})$$

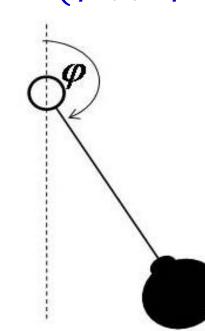


Phase Falling

Benchmark Structural-dynamic Systems

Rotating Pendulum with Free Flight Phase

$$\vec{x}_S(t) = \left(\varphi(t), \dot{\varphi}(t)\right)^T$$



$$\vec{x}_F(t) = (x(t), \dot{x}(t), y(t), \dot{y}(t))^T$$

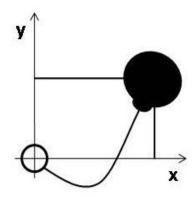
$$\vec{x}_M(t) = \left(\varphi(t), \dot{\varphi}(t), x(t), \dot{x}(t), y(t), \dot{y}(t)\right)^T$$

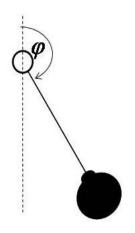
$$\vec{x}(t) = (x(t), \dot{x}(t), y(t), \dot{y}(t))^{T}$$

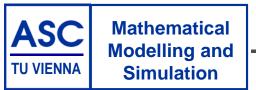


Rotating Pendulum with Free Flight Phase - Tasks

- Description of model implementations (state pace, ODEs, physical modelling,).
- Basic simulation of phases (parameter studies
- Dependency of results from algorithms (check event handling)
- External energy supply (kick pendulum dependent on state)

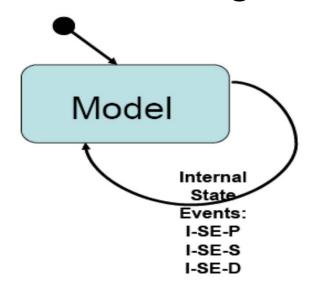




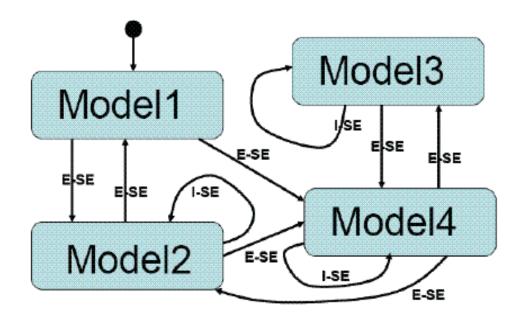


3 Case Studies

Bouncing Ball



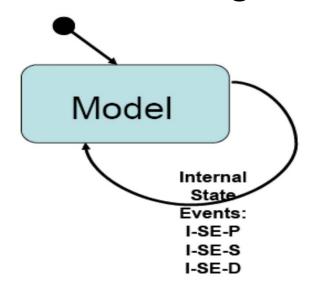
RLC Circuit with Diode





3 Case Studies

Bouncing Ball



RLC Circuit with Diode







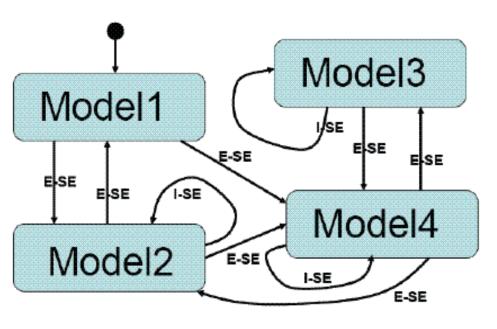


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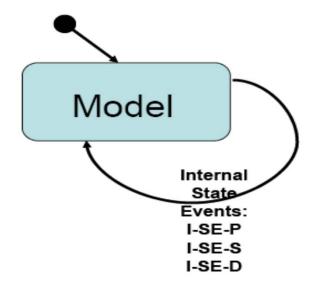




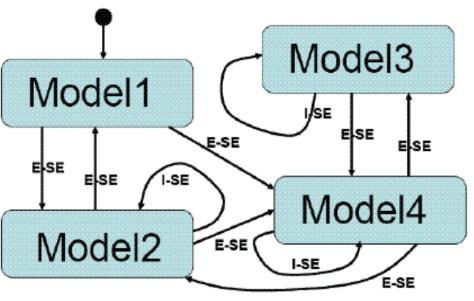
3 Case Studies

Bouncing Ball

 Solution documentation and publication in SNE of 'solutions' may take more pages – up to 10 pages SNE.





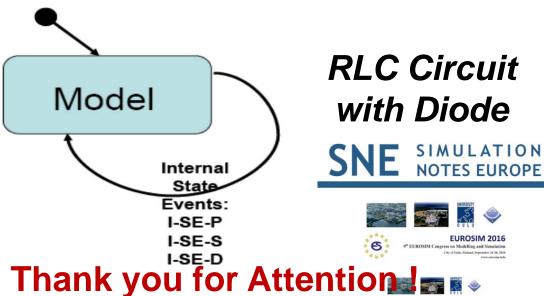


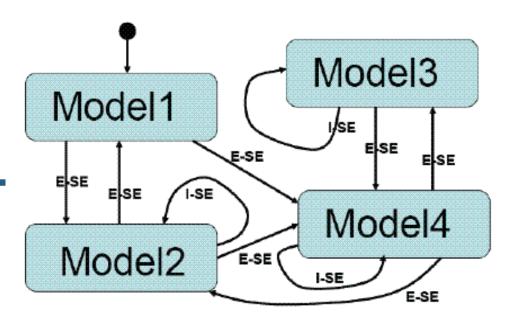


3 Case Studies

Bouncing Ball

 Solution documentation and publication in SNE of 'solutions' may take more pages – up to 10 pages SNE.





- **Happy Writing!**
- Waiting for your Submission in the state of the state of

Happy Benchmarking!